now the dynamic pressure has been calculated as low as 190. It would appear that the large differences reported by Erickson are unexpected, since both parts of the rotary inertia terms represent low-order effects.

Since one of the reasons for including rotary inertia was to attempt to account for the anomalous behavior of the curves of critical dynamic pressure vs shear flexibility for $\bar{J} = 0$ (see Figs. 5 and 6, Ref. 1), it would be interesting to see Erickson's results for these cases. The authors wish to thank Erickson for correcting the typographical errors in Eq. (23) of Ref. 1.

References

[1] Marafioti, F. A. and Johnston, E. R., Jr., "Effects of Rotary Inertia on the Supersonic Flutter of Sandwich Panels," *AIAA Journal*, Vol. 9, No. 2, Feb. 1971, pp. 245–249.

[2] Libove, C. and Batdorf, S. B., "A General Small-Deflection Theory for Flat Sandwich Plates," Rept. 899, 1948, NACA.

[3] Erickson, L. L. and Anderson, M. S., "Supersonic Flutter of Simply Supported Isotropic Sandwich Panels," TN D-3171, April 1966, NASA.

Errata: "Exhaust Characteristics of a Megawatt Nitrogen MPD-ARC Thruster"

CHARLES J. MICHELS AND DONALD R. SIGMAN
NASA Lewis Research Center, Cleveland, Ohio

[AIAA J. **9**, 1144–1147 (1971)]

IN Figs. 7 and 8, and in the text on pp. 1146 and 1147, wherever peak arc-current is shown to be equal to 7.4 kA or 13.4 kA, the values should be corrected to read 11.2 kA and 20.0 kA, respectively. Also, in the second line on p. 1145, the words "naut miles" should read nanometers.

Received July 12, 1971.